

Appendix L

A MLI model based on transient model correlation

Jan Klement Lena Bötsch Jonas Klose Christian Walker
(Tesat-Spacecom GmbH, Germany)

Abstract

Measuring and predicting the thermal heat flux through a MLI is a challenging task. A modelling approach is presented based on sectioning the MLI into different areas (Flat surface, corners and edges with and without seam). The parameters for this model are obtained using an inverse problem approach. Transient testing and model correlation is used instead of the typical steady state approach.



A MLI MODEL BASED ON TRANSIENT CORRELATION

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INTRODUCTION: THE CURRENT STATUS OF MLI MODELS

THE THEORETICAL EFFECTIVE EMISSIVITY OF AN IDEAL MLI

A theoretical ideal MLI has the thermal heat flux described by an effective emissivity between the inner and the outer layers

$$\varepsilon_{theory} = \frac{1}{\frac{2}{\varepsilon_{Al}} - 1} * \frac{1}{N + 1}$$

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THEORETICAL EFFECTIVE EMISSIVITY OF MLI

In reality this value is never reached.

There is also a huge scatter

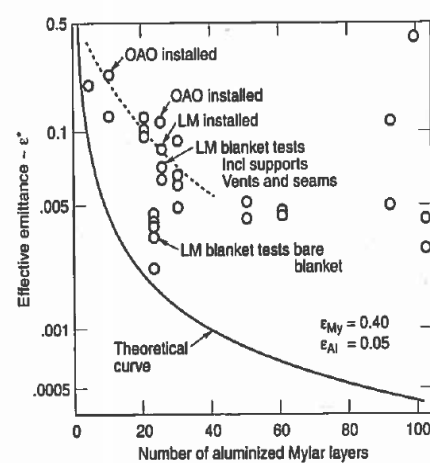



Fig. 5.3. Effective emittance vs. number of single aluminized layers.

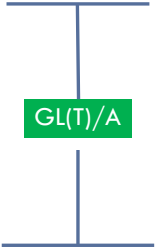
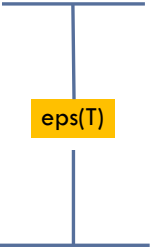
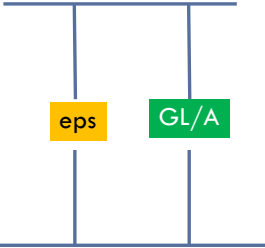
Source: David G. Gilmore, „Spacecraft Thermal Control Handbook Volume I 2nd ed“, The Aerospace Press, 2002

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TYPICAL THERMAL MLI MODEL DEFINITIONS

Temperature dependant linear conductivity	Temperature dependant Emissivity	Constant linear conductivity and emissivity in parallel
<p>Outer MLI layer</p>  <p>Inner MLI layer</p>	<p>Outer MLI layer</p>  <p>Inner MLI layer</p>	<p>Outer MLI layer</p>  <p>Inner MLI layer (chosen approach here)</p>

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TYPICAL MLI HEAT FLUX MEASUREMENT

The heat flux through an MLI is quite small. Therefore to measure these heat fluxes following is normally needed:

- » a very precise calorimeter for a large range of temperatures
- » a very stable steady state for each temperature level


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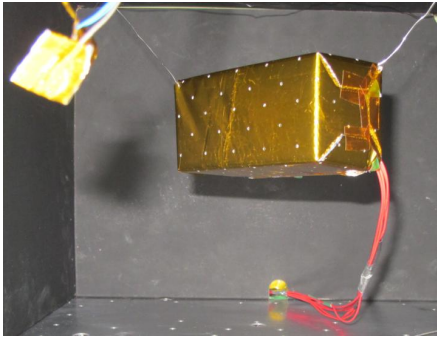
THE NEW MODEL APPROACH

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VISUALIZING THE HEATLOSS

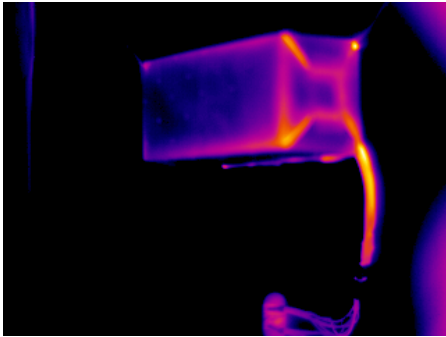
Test body packed in MLI inside TV chamber



(This MLI design is not representative)


Conclusion: corners, edges and wires have a significant contribution to the heat loss
Heat loss through the wires have to be minimized

IR picture



- Body inside the MLI is heated
- shroud is cold
- yellow = warm; black = cold

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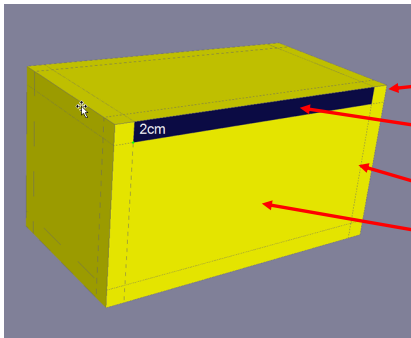


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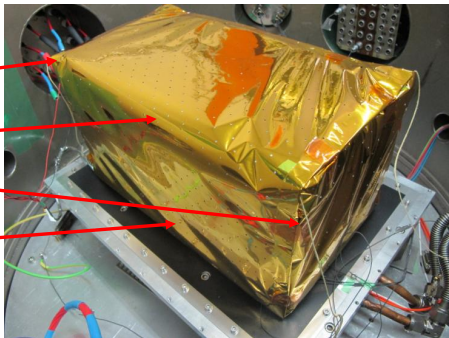
THE MODEL

The MLI is divided into 4 areas
The edge area is defined as 2cm wide

Thermica GMM



hardware



corner

Edge closed

Edge overlapping

Flat area

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The 7 test bodies with very different dimensions are used. One is tested with different 2 MLI configurations (7 and 12 overlapping edges). 8 tests in total





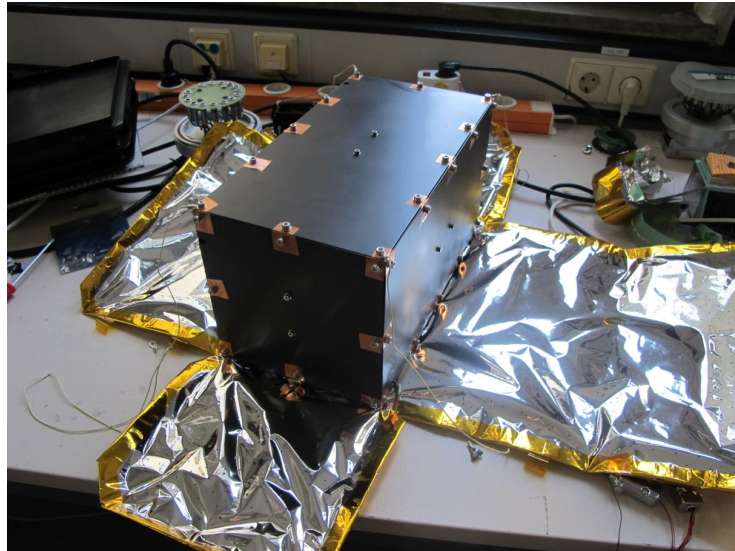




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THE APPROACH

- » 7 bodies made out of copper are packed in
 - » 15 (Mylar VDA on both sides)
 - » 2 (Kapton) layer MLI



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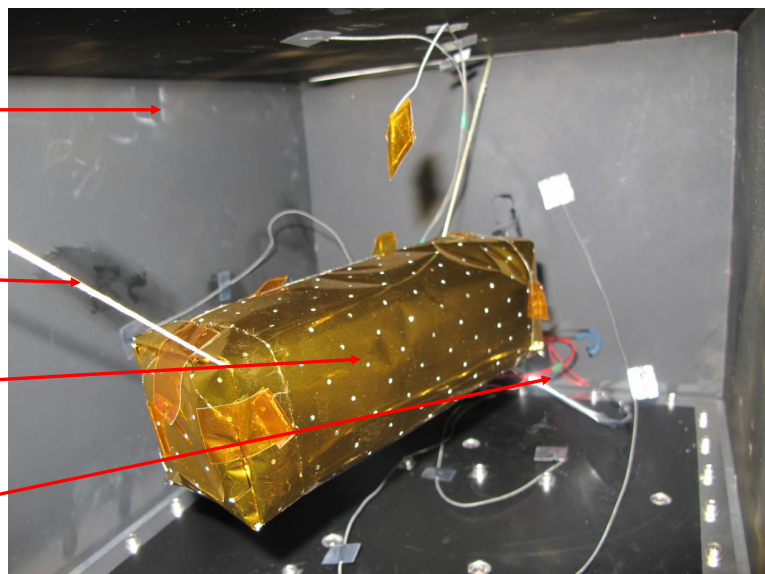
TEST BODY IS PLACED IN THERMO VACUUM CHAMBER

Shroud controls the environment temperature

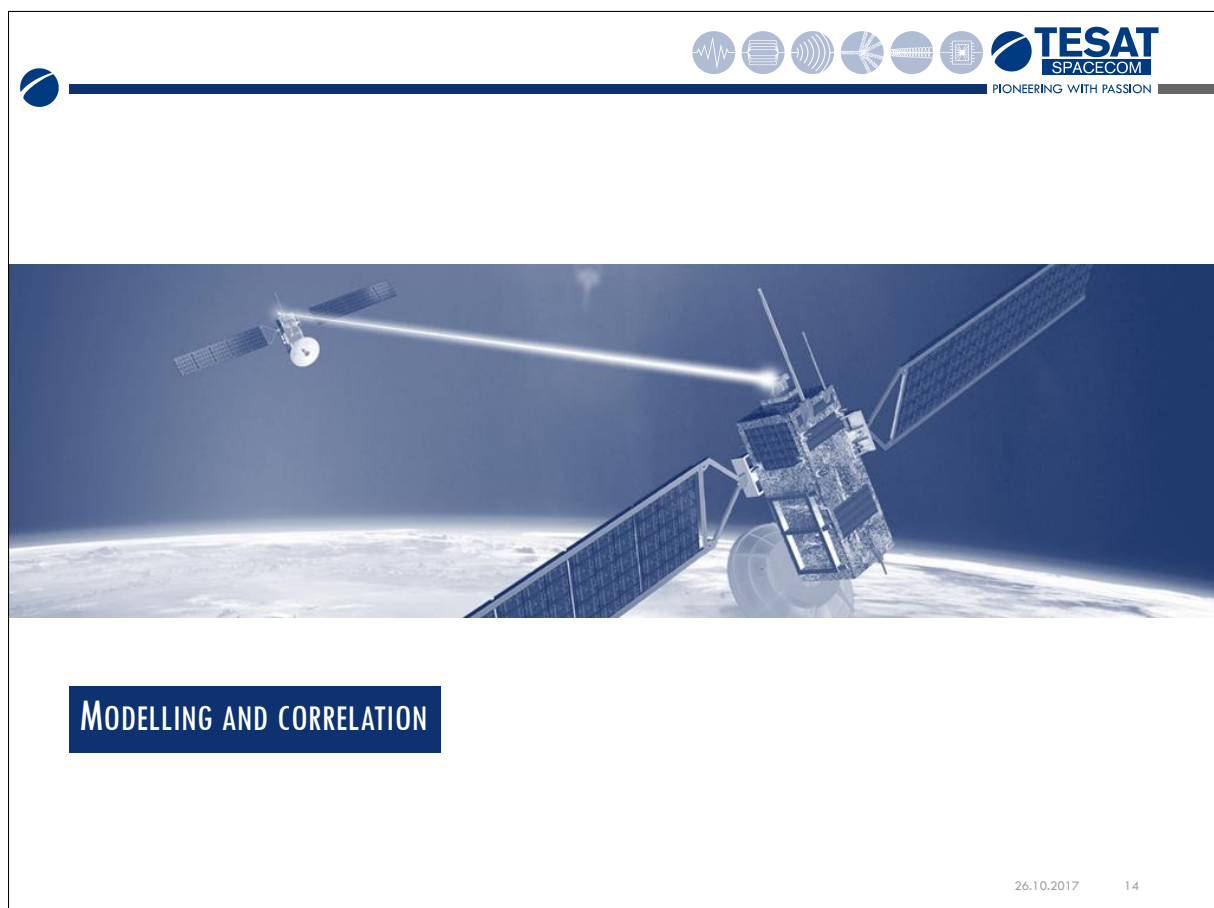
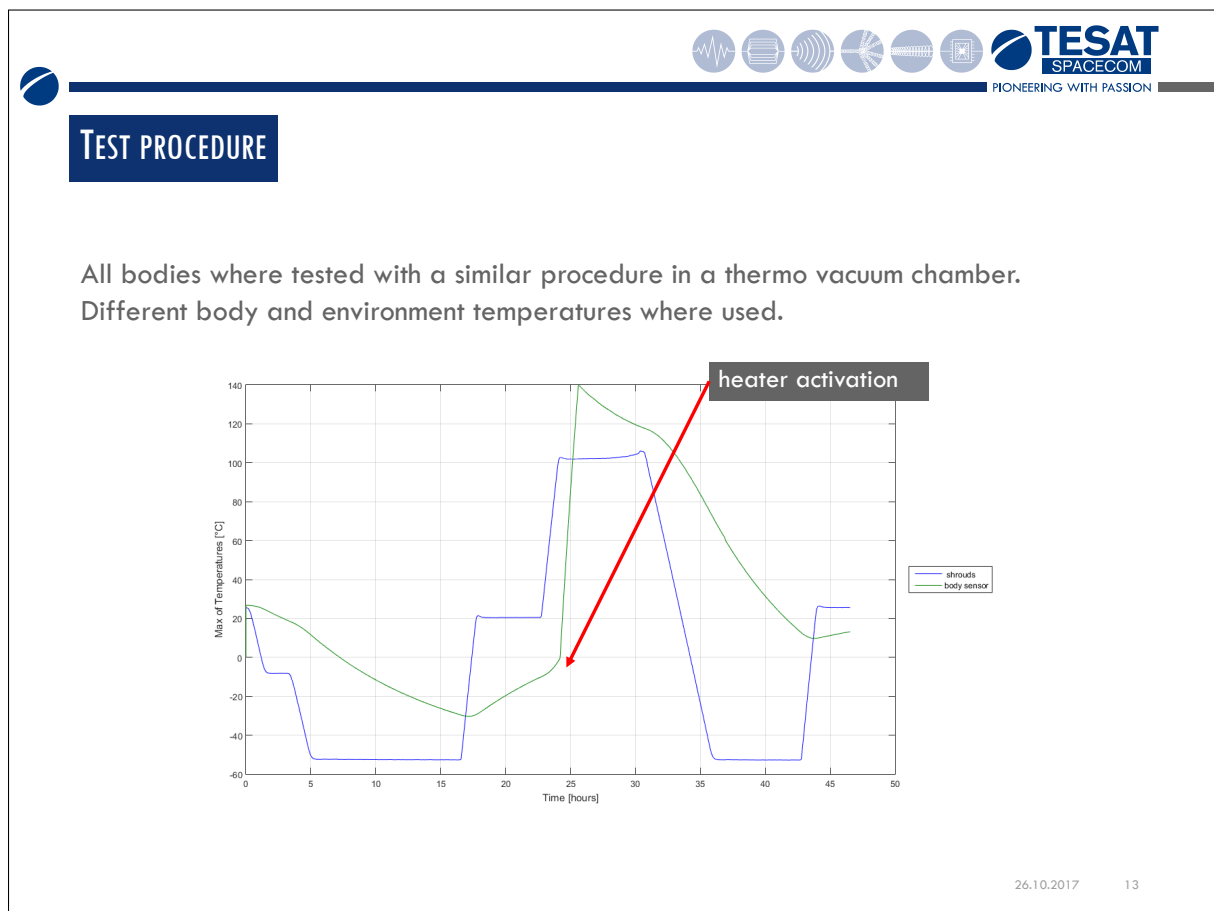
Supported only by Kevlar strings

Test body in MLI

Thin wires for the heaters and one temperature sensor

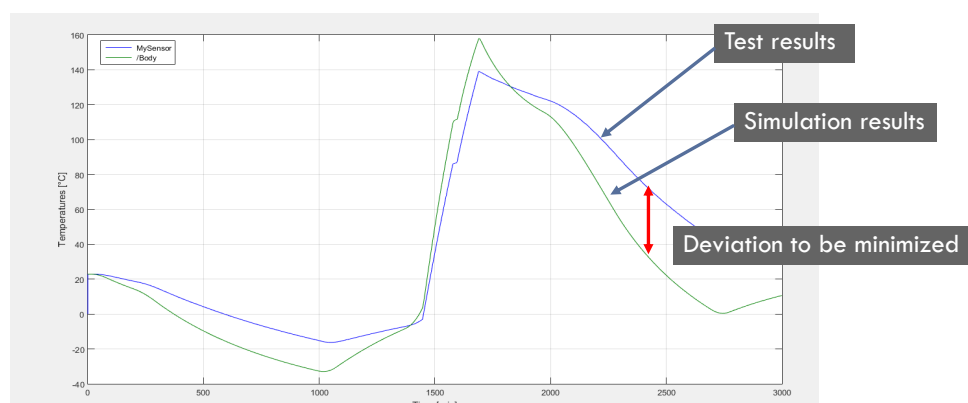


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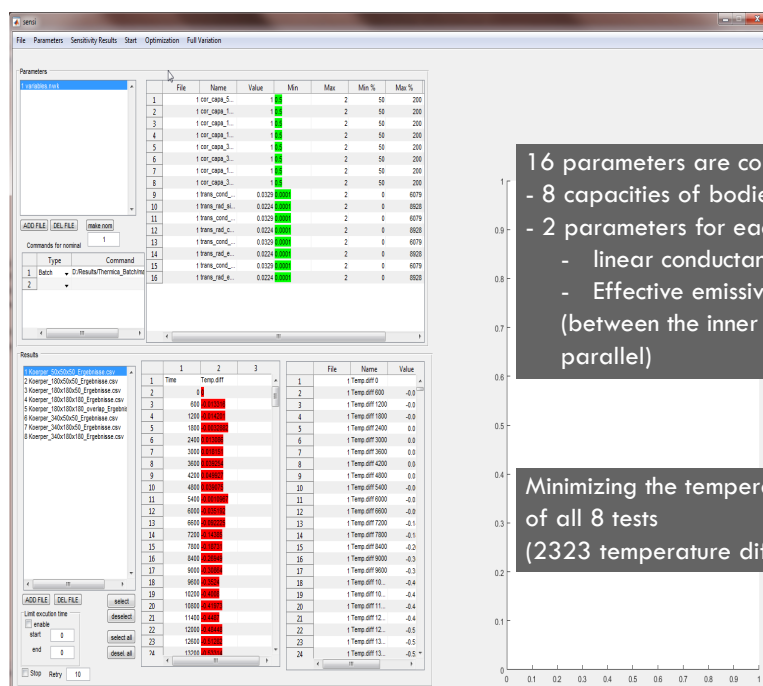
COMPARISON TO SIMULATION (BEFORE CORRELATION)

All tests were simulated in Thermica using typical values.
 The shroud temperature from the has been mapped onto the shroud nodes.



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CORRELATION SOFTWARE (DEVELOPED AT TESAT)

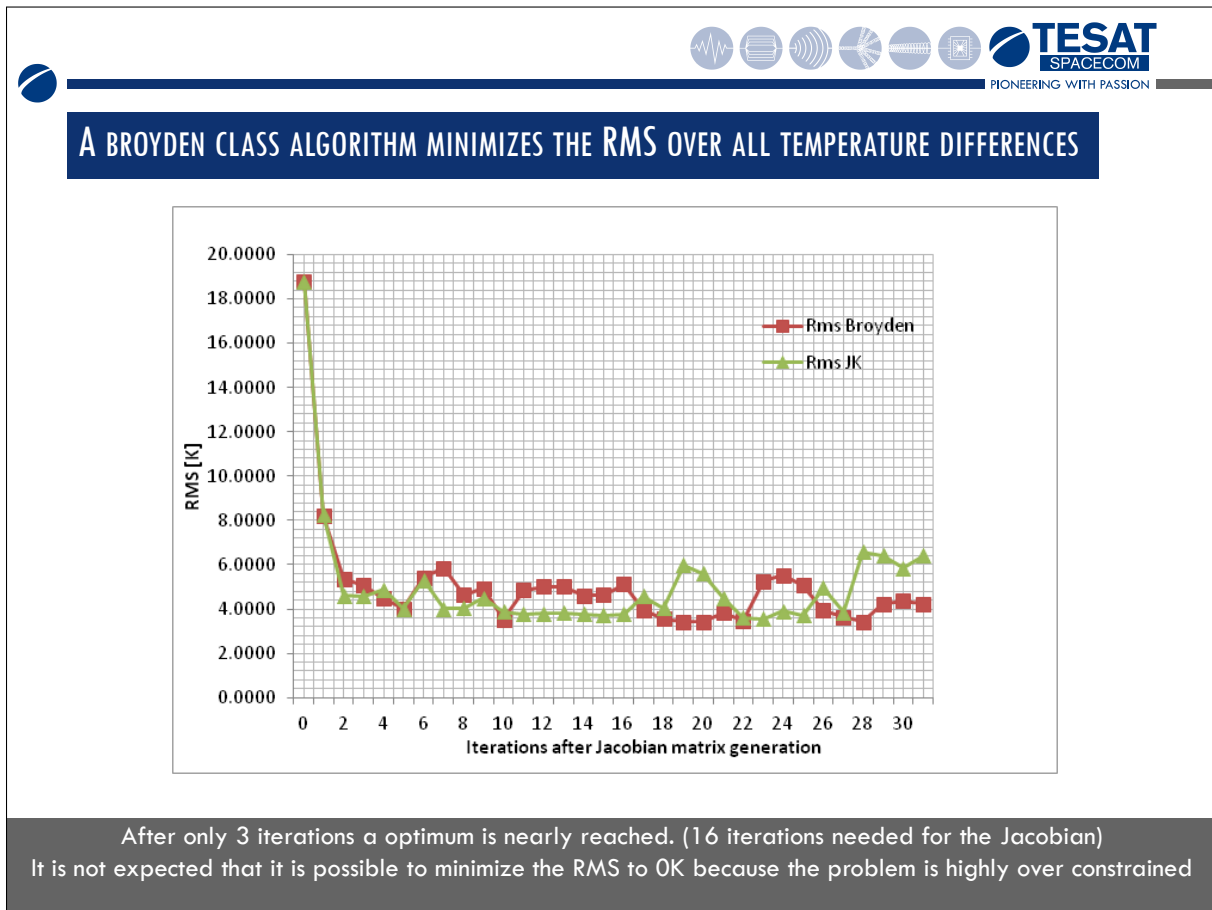


16 parameters are correlated

- 8 capacities of bodies
- 2 parameters for each MLI area
 - linear conductance W/Km^2
 - Effective emissivity (between the inner and outer MLI layer in parallel)

Minimizing the temperature differences of all 8 tests (2323 temperature differences in total)

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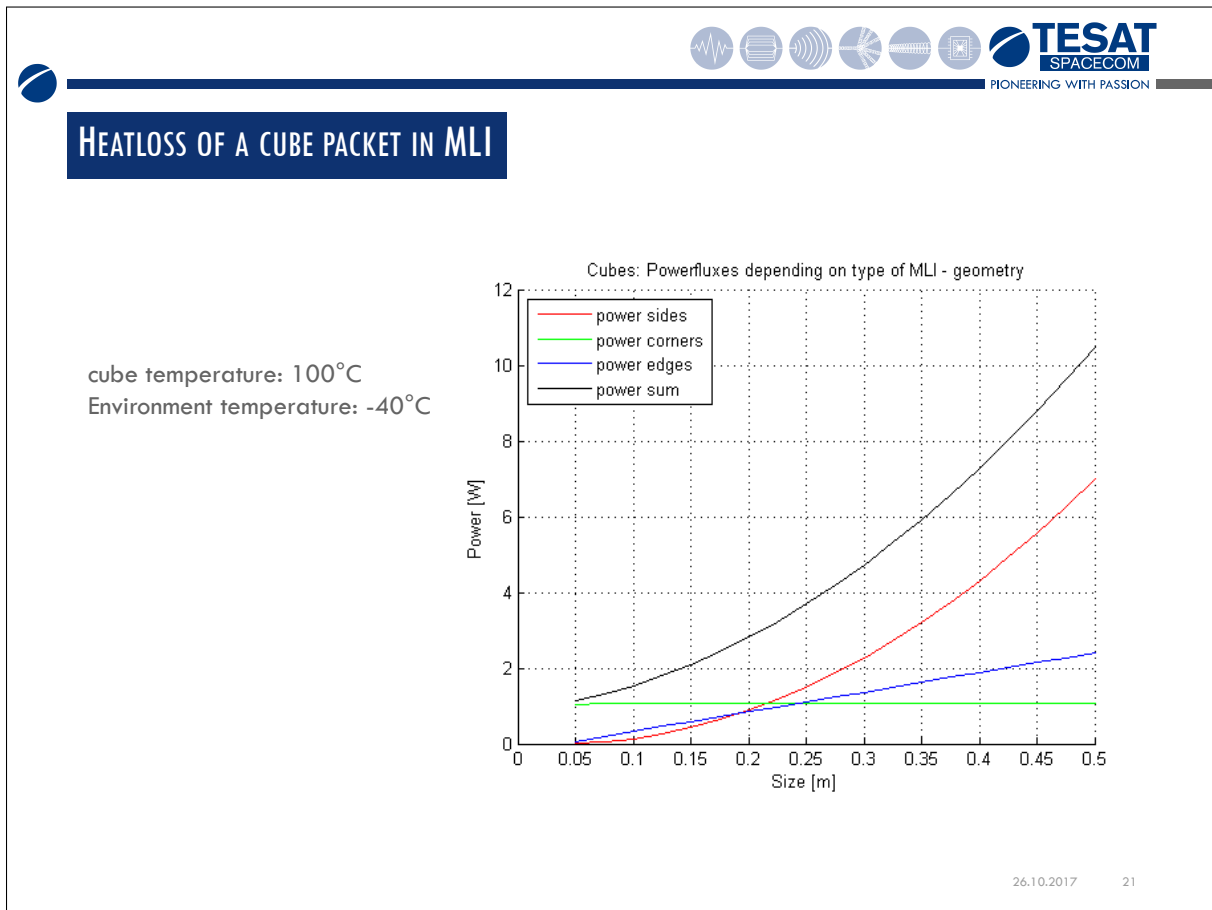
RESULTING MLI PARAMETERS FROM THE CORRELATION


Parameter	Effective conductivity*	Effective emissivity*
Flat area	0.004445 W/m ² K	0.003365
Corners	1.013198 W/m ² K	0.000179
Closed Edges (only bent)	0.000101 W/m ² K	0.014994
Edges with overlapping MLI	0.264138 W/m ² K	0.007348

*) The conductivity and the emissivity must be used in parallel between the inner and outer layer.

These are effective nominal parameters. They fit to the results but their temperature dependency may not be accurate. The corresponding assessment of their accuracy is to be discussed tomorrow.

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CONCLUSION

- » The advantages of transient testing are:
 - » No complicated and precise calorimeter is necessary
 - » Temperatures changes are used which can be measured quite accurate
 - » It is not necessary to wait until steady state is reached
 - » Each test gives a information for whole range of temperatures instead of one single point
 - » Only one temperature sensor is necessary inside the body

In other words: More data with an easier, faster and cheaper test.

- » Correlation
 - » Broyden class algorithms needed only a few(<20) iterations to reach an optimum (transient model, 16 parameters, 8 configurations & tests, 2323 temperatures differences)

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OUTLOOK

- » The method can be used to extend the MLI model for:
 - » Different corner angles
 - » Stand-offs
 - » Flaps
 - » Slits
 - » Different layer setup
 - » Larger bodies
- » With more extreme temperatures the temperature dependency can be analyzed with higher accuracy.
- » The correlation software(Sensitool) can be obtained by other companies of the Airbus Group

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THANK YOU

Gefördert durch:



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für Wirtschaft
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