

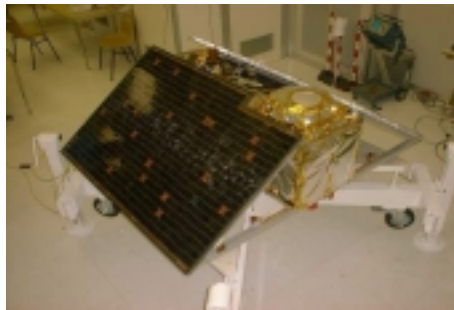
## Data exchange between SINDA/FLUINT and MAYA/TMG for a payload thermal control design: NINA and MITA

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## MITA minisatellite - an overview

- MITA is an Italian Space Agency (ASI) project for the development of a standard satellite platform, supported by Carlo Gavazzi Space as the Prime Contractor. The aim of the project is to develop a low cost, **modular** and **flexible** platform, 200 [kg] class, to support several kind of small missions: scientific, technological, Earth observation, communication.



### FEATURES

Low recurring costs (5 MEU\* \* 1999 economic conditions )

Bus modularity

Fast implementation of the mission (typical C/D phase duration: 18 months)

Compatibility with different payloads (several A-phase successfully performed)

Compatibility with different launchers (Cosmos, Start, Pegasus, Vega, Delta)

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## NINA Payload

- In this mission MITA will carry the **NINA** payload, a silicon particle detector provided by INFN (Italian Institute of Nuclear Physics). The detectors are stacked to build up the tower.



**NINA tower  
(without vessel)**

- NINA is able to detect charged particles in the 12-100 MeV range.

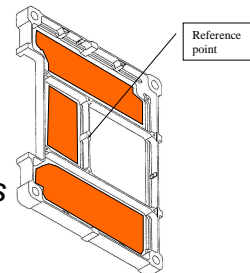


**NINA (with vessel)**



## NINA payload thermal requirements

- *The silicon detector, installed on an aluminium frame (see figure) cannot be outside the range  $0^{\circ}\text{C} \div +25^{\circ}\text{C}$*
- *A thermal control of the whole tower (made of stacked frames) by means of heaters / thermostats was designed in an iterative way*





## MITA and NINA modelling standard

- MITA SATELLITE: *MAYA TMG*
- PAYLOAD: *SINDA/FLUINT*
  - *A direct include of the NINA model in TMG was accomplished by means of a reduced model, lumping the thermal characteristics of NINA in a few nodes that were included in the large satellite model.*
  - *The NINA thermal control sizing was done on the NINA detailed model*



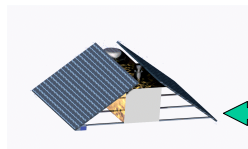
## DATA EXCHANGE

TMG

- Model size: >1000 nodes
- Average power budget for the heaters

SINDA/FLUINT

- Thermostats set point in the detailed model
- Time dependent heater power in the detailed model



Similar temperatures!!

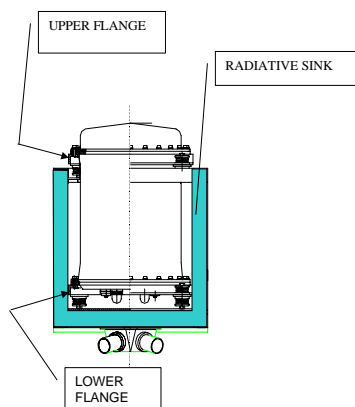


## ENERGY CONSERVATION

- The average heater power put on NINA tower model has to be taken into account in the general satellite model
- The detailed model is used to locate precisely the thermostats and to calculate the average power dissipated by the heaters: a transient analysis is performed letting heaters switching on and off
- The reduced model provides the information how the heat power is distributed to the satellite structure by radiation /conduction
- A final check is done comparing the solutions obtained running the NINA complete model alone and the MITA satellite complete model



## NINA reduced thermal model (1)



The NINA thermal control is based on radiation heat rejection on the satellite bus lateral/rear walls.

The NINA vessel is fixed to the satellite structure by means of dampers, with a low thermal conductivity (0.1 W/K each).

- 4 dampers are located on the upper NINA flange
- 4 dampers are located on the lower NINA flange

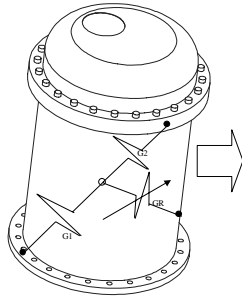
Payload thermal control design:

NINA and MITA

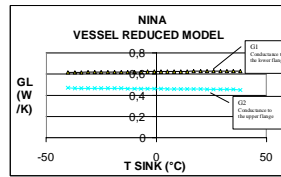
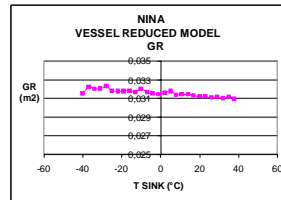


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# NINA reduced thermal model (2)



The NINA thermal model has been reduced to a simple network with 2 GL and 1 GR, temperature dependent. The sink temperatures have been used as free parameters for calculating the reduced model conductances.



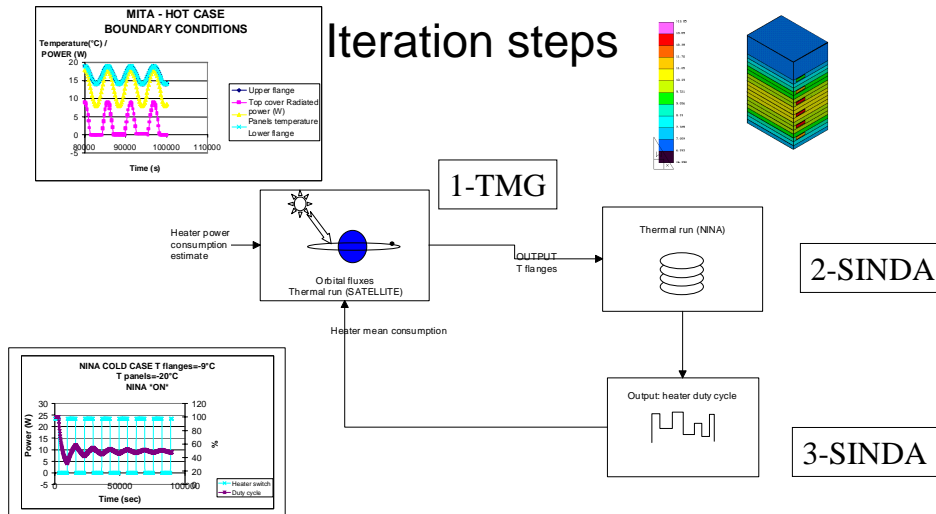
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Payload thermal control design:

NINA and MITA



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## Iterations description

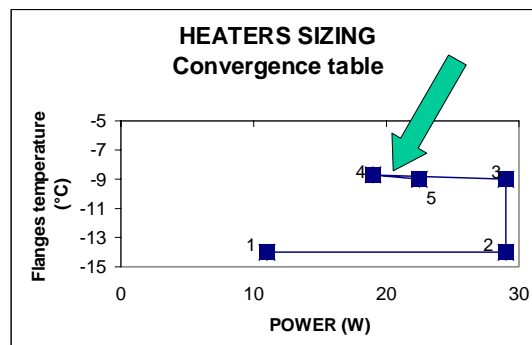
- 1) Orbital loads are calculated and MITA model is run (TMG)  
TMG gives TRANSIENT sink temperatures (radiative and conductive) for NINA;
  - 2) The detailed NINA thermal model is run (SINDA) using the actual sink, time varying - Thermostats are sized and
  - 3) The average power dissipation (duty cycle) is calculated and given back to the general MITA thermal model
- \*\*) If temperatures obtained at point 1) are within 1°C the one obtained at point 2), the iteration is stopped

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## HEATERS SIZING

### DESIGN POINT:

- Flanges temperature = -9°C
- Heaters power = 20 W

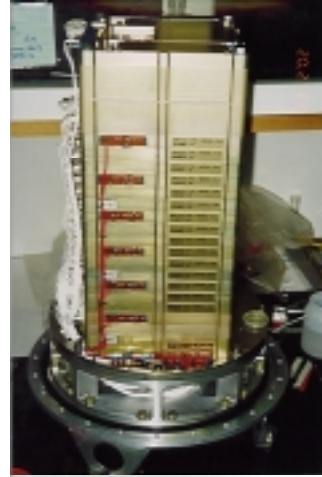


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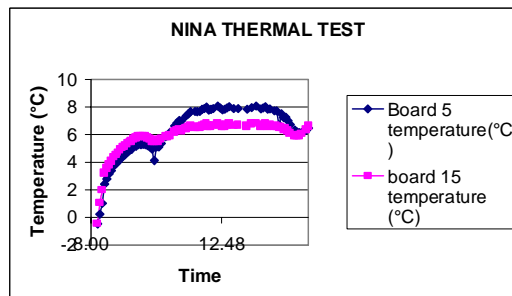
## Heaters and thermostats installation

- Hardware implementation:
  - HEATERS: 6 x 3.8 W= 23 W
  - THERMOSTATS: NORMALLY OPEN, CLOSSES @ 3 °C ±2.2 °C



## NINA thermal tests

- NINA thermal tests in air allowed to validate the NINA modelling: the outer temperature was at -9°C: the boards remained over 6°C.

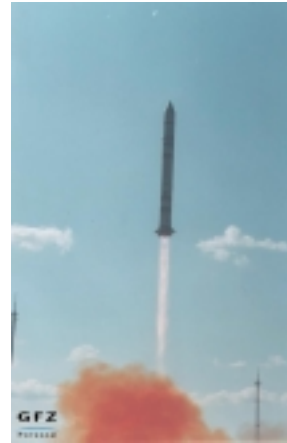


- The thermostats are located on the tower coldest point.



## MITA launch

- 15/7/00
- 12.00 GMT
- Plesetsk Kosmodrom
- Temperature at launch  
25°C
- ORBIT:  $i = 87^\circ$ ,  $h = 450$  Km



## MITA THERMAL MODEL

- *In the commissioning phase a MITA thermal model was built in SINDA, confirming that the above mentioned approach was providing a correct description of the payload-to-satellite heat exchange mechanisms (with less than 1°C between the complete and the reduced model), but showing moreover that the lumped parameter approach allows a better tuning of the model, when experimental data are available.*





## MITA MISSION PHASES

- LAUNCH - DEPLOYMENT
- After deployment:
  - SAFE MODE (SUN POINTING)
  - NOMINAL MODE (NADIR POINTING)
    - Thermally affected by Beta angle changing from 0° to 90° due to orbit precession.

In all the following graphs are plotted

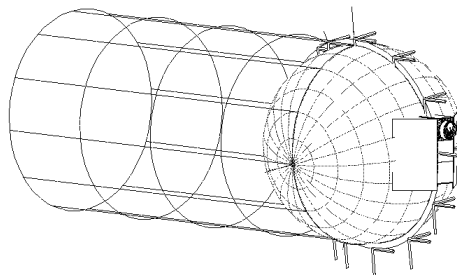
- the NINA vessel temperature
- the radiator temperature (sampled in two points).



### SAFE MODE (SUN POINTING inertial attitude, $\beta=20^\circ$ )

•In the sun pointing attitude the radiator always faces the deep space.

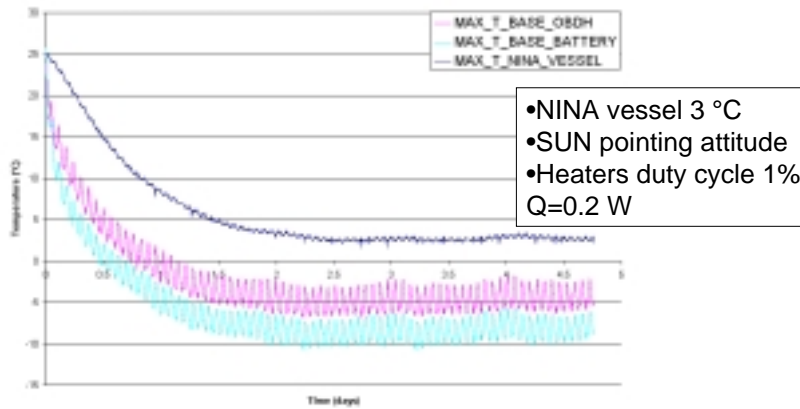
•For this reason, even if this attitude was combined with a hot beta angle, the NINA temperatures were at their lower limit.





NINA thermal behaviour on orbit (1)

# STABILIZATION AFTER LAUNCH



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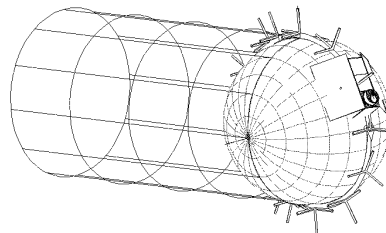
NOMINAL MODE (1)

# (Nadir pointing attitude, $\beta=0^\circ$ )

- ACTUAL HOTTEST CASE
- Beta=0° (10<sup>th</sup> August 2000)

HOT DIMENSIONING CASE Beta=0°

NINA temperature  
between 10°C and 15°C  
Heaters OFF



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Payload thermal control design:

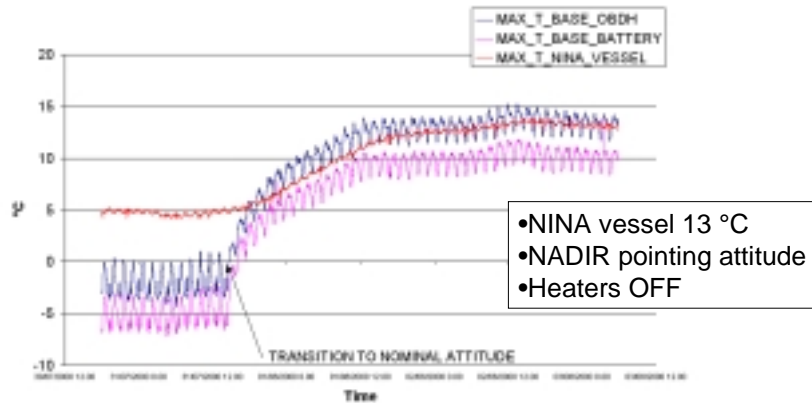
**NINA and MITA**



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NINA thermal behaviour on orbit (2)

# TRANSITION SUN POINTING NOMINAL



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Payload thermal control design:

**NINA and MITA**



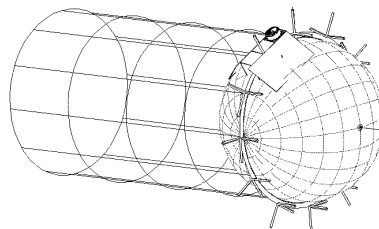
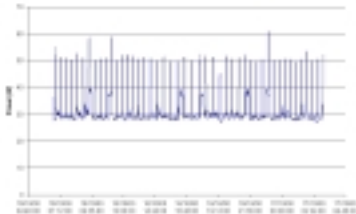
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NOMINAL MODE (2)

## (Nadir pointing attitude $\beta \sim 90^\circ$ )

- ACTUAL COLDEST CASE:  
Beta=82°  
(20th October 2000)  
In this case the heaters are switching on and off (see below)

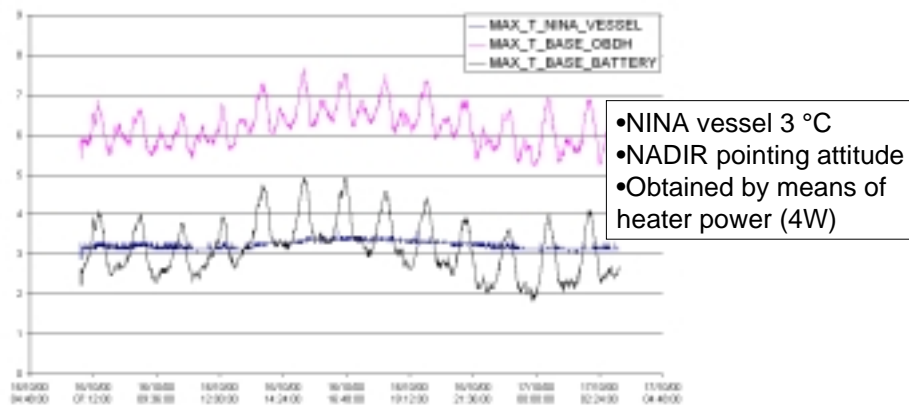
COLD DIMENSIONING CASE  
Beta=90°



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## NINA thermal behaviour on orbit (3) COLDEST ORBIT - NADIR POINTING



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## NINA thermostats operations

- Heaters switch on (at  $\beta \sim 90^\circ$ )
- Average heater power = 4 W (due to flanges temperatures hotter than predicted (1°C instead of -9°C))
- NINA temperature is kept at  $\approx 3^\circ\text{C}$  by heaters

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## CONCLUSIONS

- The data exchange between SINDA and TMG models is possible making accurate reduced models;
- The model can be run using transient interface data;
- The thermal control is providing excellent performance, confirming models predictions.